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# Processes involving gases in valve-regulated lead/acid batteries

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#### Abstract

The kinetics of  $O_2$  and  $H_2$  reactions with the active mass of the plates have been investigated by carrying out open-circuit and overcharge tests on cells and plates coming from commercial valve-regulated lead/acid batteries of different producers. The tests at open circuit showed that the rate of  $O_2$  reduction at the negative plates is about four orders of magnitude higher than that of the other four reactions examined (evolution of  $O_2$  at positive plates and of  $H_2$  at freshly charged negatives,  $H_2$ consumption at positive and partially discharged negative plates).  $H_2$  leaking through the battery walls, which showed a permselective membrane behaviour, was also considered. Overcharge tests allowed the mathematical model proposed elsewhere to be verified and provided information on the cell behaviour when the overcharge current became equal or lower than the  $O_2$ reduction limiting current. The experiments on single plates and on couples (1 positive and 1 negative) sealed in glass vessels showed that the cell construction has a strong influence on the rate of gas-recombination processes.

Keywords: Valve-regulated lead/acid batteries; Hydrogen; Oxygen

## 1. Introduction

The main feature of valve-regulated lead/acid batteries (VRLA), in which the acid is gelled or retained in a microfibre glass mat, is their capability of consuming the gases evolved during service, so that the container can be in principle completely sealed.

The literature reports a number of papers on this subject. Together with review articles [1-4], there are some more specific ones dealing with the behaviour of commercial systems [5,6], with the definition of a method for the recombination-efficiency evaluation [4,7–9] and with the kinetics of processes regarding O<sub>2</sub> [4,10,11] and H<sub>2</sub> [12–14].

Fundamental studies on  $H_2$  and  $O_2$  reactions in a gas-recombining system have already been carried out by our group [15–19]. An experimental method based on the monitoring of the cell internal pressure was developed in order to determine the kinetic constants of  $H_2$ - and  $O_2$ -consumption reactions [17].

Through preliminary investigation the reliability of the proposed model was verified, showing that the kinetic constant of  $O_2$  reduction at the negative is much higher than that of  $H_2$  oxidation.

The results of such preliminary tests clearly indicated that a correct analysis of gas-recombining cells must include, in addition to  $O_2$  reduction, the following processes: (i)  $H_2$  leakage through the plastic walls; (ii)

0378-7753/95/\$09.50 © 1995 Elsevier Science S.A. All rights reserved SSDI 0378-7753(95)02188-M  $H_2$  oxidation, and (iii) spontaneous  $O_2$  evolution, both at the positive plates [18,19].

In this work we have extended the test duration to 500–1000 h and applied gas chromatographic analysis to establish the composition of the gaseous mixture during overcharge and hence obtain information on the occurring processes.

# 2. Basic theory

The developed model [17,18] describes the behaviour of gas-recombining lead/acid batteries submitted to a constant overcharge current I. It considers a fully charged cell in a sealed container at a given temperature T and a free volume V, initially filled with some gaseous species (air or O<sub>2</sub> or H<sub>2</sub> or N<sub>2</sub>).

The processes involving the gaseous species present in the free volume are indicated in the scheme of Fig. 1. The gas reactions are coupled with  $PbO_2$  or Pb sulfate.

The material balance of the various gases is described by the following simultaneous differential equations:

$$dN_{\rm O}/dt = I_{\rm O}/4F - K_{\rm O}N_{\rm O} + f_{\rm O}$$
(1a)

 $dN_{\rm H}/dt = I_{\rm H}/2F - K_{\rm H}N_{\rm H} + f_{\rm H}$ (1b)

$$dN_{\rm N}/dt = f_{\rm N} \tag{1c}$$

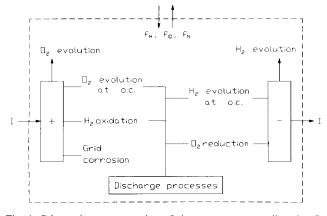


Fig. 1. Schematic representation of the processes regarding the  $O_2$  and the  $H_2$  cycles in a VRLA cell; o.c. = open circuit.

where  $N_{\rm O}$ ,  $N_{\rm H}$  and  $N_{\rm N}$  are the oxygen, hydrogen and nitrogen numbers of moles in the free volume V of a cell,  $K_{\rm O}$  and  $K_{\rm H}$  the kinetic constants of O<sub>2</sub> reduction and H<sub>2</sub> oxidation.  $f_i$  (*i*=O, H, N) is a parameter, accounting for the gas transfer into and out of the battery through leaks in the container, which depends on the internal pressure value.  $I_{\rm H}$  and  $I_{\rm O}$  are the rates, expressed as an electrical current, of H<sub>2</sub> and O<sub>2</sub> evolution. These current intensities are calculated [19] taking into account both the external current *I*, the rate of the plates discharge caused by gas reaction, and that of the positive grid corrosion.

If we take T and V constant and the gaseous species as ideal gases, their numbers of moles can be expressed as partial pressures. The kinetic constants can be determined from the internal pressure monitoring at open circuit or from the gas composition analysis in a cell maintained under galvanostatic conditions. In addition,  $K_{\rm O}$  can be obtained from the measure of the limiting current of oxygen reduction at the negative plate which is equal to  $4FK_{\rm O}N_{\rm O}$  [17,19].

The kinetic constants of the  $O_2$ - and  $H_2$ -consumption reactions can be used to evaluate the amount of the water lost by a cell during overcharge, by calculating the volume of gas escaped through the pressure vent.

If the gas-consumption reactions occur under limiting current conditions, [20–23],  $K_{\rm O}$  and  $K_{\rm H}$  are not dependent on the plate potential. Their values are affected by the extent of the total active surface of the plates and by the internal free volume of the cell, as the gas concentration at the reaction sites depends on the gas pressure, that is on the  $N_i/V$  (i=O, H, N) ratio. So, aiming to compare batteries having different geometry, we consider the specific kinetic constants  $K_{\rm Os}$  and  $K_{\rm Hs}$ defined by:

$$K_{\rm Os} = K_{\rm O} V / S_{\rm n} \tag{2a}$$

$$K_{\rm Hs} = K_{\rm H} V / S_{\rm p} \tag{2b}$$

In the case of  $O_2$  reduction, it is of some interest to introduce the merit factor  $\Gamma_0$  defined as the ratio between  $K_{OS}$  for a complete cell and  $K_{OS}$  for a couple of plates (one positive and one negative) coming from the same cell. The  $\Gamma_O$  value depends only on the fraction of the negative plate which is active to O<sub>2</sub> reduction.

# 3. Experimental

The four types of batteries used in the tests are commercial stationary VRLA batteries coming from different manufacturers (Yuasa Battery Company, Tudor, Chloride Ltd., and FIAMM SpA). All of them have the electrolyte supported by glass-fibre separator, the voltage ranges from 6 to 12 V, the capacity between 50 and 100 Ah.

The batteries, three for each type, were preliminary checked according to the procedure reported in Ref. [17]. The cells of each battery were equipped with an electronic pressure sensor and tests on the vent plugs carried out.

The cells were then prepared for the internal free volume measurement and the subsequent tests [17]. The pressure monitoring, at open-circuit or in galvanostatic conditions, was performed with the case free volume initially filled with a known gas (air or  $O_2$  or  $H_2$  or  $N_2$ ), according to the procedure described in Ref. [18]. The tests lasted from 500 to 1000 h. When needed, gas chromatografic analysis of the internal gas mixture was performed.

Tests on single plates and on couples, consisting of one positive and one negative plate, were also run. The plates, coming from the disassembling of batteries of the same kind of those tested, were charged before the tests and left immersed in 1.28 g/cm<sup>3</sup> sulfuric acid for 1 h. After 1 min dripping, they were finally sealed in a glass container having a total volume of 400 cm<sup>3</sup> and equipped with a pressure sensor. The couples were assembled, just before introduction into the vessel, with the interposition of a polyethylene separator between the plates. In some cases plates were wetted again during the tests: they were taken out of the vessel, immersed in the H<sub>2</sub>SO<sub>4</sub> solution for 1 h, left to drip for 1 min and then sealed again.

All the tests were carried out at room temperature (23-28 °C) and all reagents were of analytical grade.

Particular attention was paid in preventing and controlling gas leakage, especially  $H_2$ , through the connections of the cells under test. The empty battery cases used for the determination of  $H_2$  loss through the plastic container wall were previously tested by monitoring their internal pressure after filling with  $N_2$ (see Fig. 7, curve (b)). The same Figure reports, curve (c), the behaviour of a glass container filled, after control of its connections, with  $H_2$  only.

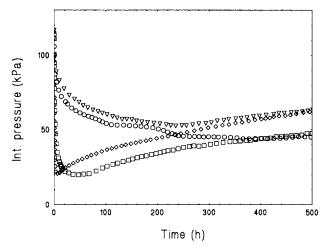


Fig. 2. Pressure vs. time plots for cells of the four battery types under test. All the cells, fully charged, were at open circuit and initially filled with pure  $O_2$ .

Chemical analysis of the active mass was always performed on the negative plates coming from a just disassembled battery.

#### 4. Results and discussion

#### 4.1. Open-circuit tests

#### 4.1.1. Oxygen reduction at the negative plate

The internal pressure of the four types of cell, fully charged, at open circuit and filled with pure  $O_2$ , decreases with time as shown in Fig. 2. The initial rapid decay of pressure is related to the reduction of  $O_2$  on the lead sponge of negative plates [15–17]. It is followed by a pressure increase due to  $H_2$  evolution on lead. The curves show that, in some case, the two concurrent phenomena give origin to a well-defined minimum.

Under similar experimental conditions (open circuit and filling with  $O_2$ ), the different couples of plates in sealed glass containers showed a very similar behaviour, an example is reported in Fig. 3. Analogous results were obtained by single negative plates in pure  $O_2$ . The uniformity of these findings indicates that the differences in the curves of Fig. 2 must be ascribed to features of the battery other than the plates characteristics. The percentage of free pores in the separators, the plates compression, the amount of electrolyte, the amount of the free volume and the number of plates have a marked influence.

The values of the specific kinetic constant  $K_{Os}$  range between the following values:

(i) 0.9-1 cm/h for single negatives and positive/negative couples, and

(ii) 0.02–0.1 cm/h for complete cells.

These values well agree with those obtained measuring the O<sub>2</sub>-limiting current,  $I_{\text{lim}} = 4FK_{\text{Os}}N_{\text{O}}S_{\text{N}}/V$ .

100 100 Int. pressure (kPa) 50 50 <u>200 0 00 0</u> 77 0 0 100 200 300 400 500 Time (h)

Fig. 3. Pressure vs. time plot for a couple of positive and negative plates, coming from the same battery, at open circuit in a sealed glass container filled with pure  $O_2$ .

The merit factor  $\Gamma_{\rm O}$  ranges between 0.022 and 0.11 showing that, in the cells, the extent of the plate active surface is greatly reduced.

Analysis of the experimental data indicates that the pressure-time curves follow an exponential law in the initial part of the decay only (up to 1 h in the case of cells), that is well before the attainment of the pressure minimum. This is verified for single negatives, couples of plates and complete cells. One can thus exclude the influence of diffusion phenomena in the gaseous phase or the effect of the amount of acid.

A possible explanation is that the pressure decay trend is influenced by the formation of a  $PbSO_4$  barrier layer on the surface during  $O_2$  reduction, partially blocking the sites where oxygen reacts [4]. To verify this hypothesis, the test concerning  $O_2$  reduction on the negative plate has been repeated several times on the same sample, without wetting with acid at every new run. In the end, before the final test, the plate was wetted with acid and the test carried out. It can be seen, Fig. 4, that the first three pressure decays exhibit a standard trend while the fourth is markedly modified. The last one, with plate rewetting and  $O_2$ refilling, is again similar to the first three decays, although the decay is here slower.

As the first three decays are practically identical, while the amount of  $PbSO_4$  is progressively increasing, the  $K_0$  variation cannot be ascribed to the formation of a sulfate barrier layer. The lower rate at which the fourth decay takes place is probably due to a lack of sulfuric acid as suggested by the calculations of the quantity of acid consumed at each decay. In fact rewetting with acid restores the initial conditions.

The non-exponential part of the pressure decay, following the initial exponential one, could be due to water flow, produced by the  $O_2$ -reduction reaction, from inside of the pores of the active mass towards the

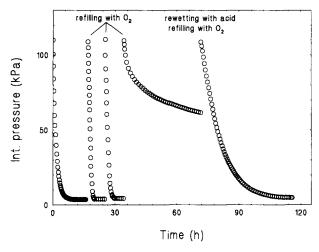


Fig. 4. Pressure decay vs. time for a negative at open circuit in a sealed glass container repeatedly filled with pure  $O_2$ .

outside. Another reason could be the rapid increase of the surface temperature. Such a temperature rise reduces the  $O_2$  solubility and causes water evaporation which visibly condenses on the glass walls. Finally, as a variation of the cell potential has been observed during oxygen reduction at open circuit, it is possible that, opposite to what is outlined in the literature [20–23],  $O_2$  discharge does not take place in limitingcurrent conditions so being influenced by the potential variation.

## 4.1.2. Other gas-involving processes

The other processes that modify the internal pressure of a VRLA cell at open circuit proceed at a much lower rate. Investigations on single plates put in evidence four reactions at open circuit, three of them regarding  $H_2$  and one  $O_2$ .

The  $O_2$ -evolution rate at the positive plate at open circuit can easily be detected from internal gas analysis and pressure monitoring in a vessel, containing a single positive, initially filled with pure  $N_2$  or pure  $O_2$ , Fig. 5 curves (a) and (b). The slope of the curves directly provides the reaction rate  $v_s$  whose value, referred to the unit of free volume and plate surface, is reported in Table 1.

Considering a positive plate in a sealed glass cell filled with pure H<sub>2</sub>, the pressure decrease, Fig. 5 curve (c), is due to the two processes of O<sub>2</sub> evolution and H<sub>2</sub> consumption. If the effect of O<sub>2</sub> evolution is eliminated from curve (c), the pressure decrease follows an exponential law from which it is possible to get the  $K_{\rm H}$  value for H<sub>2</sub> consumption at the positive, Table 1.

As for the negative plate, the spontaneous  $H_2$  evolution is the process which controls the internal pressure of a glass case containing a single negative filled with  $N_2$ , Fig. 6 curve (a). If the vessel is initially filled with  $O_2$ , Fig. 6 curve (b),  $H_2$  evolution comes in evidence when all  $O_2$  is exhausted. The  $H_2$ -reaction rate, Table 1,

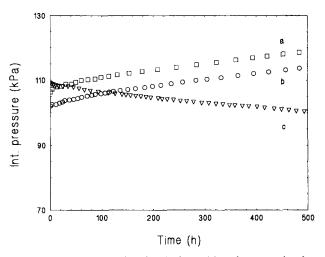


Fig. 5. Pressure vs. time plots for single positive plates, coming from the same kind of battery, sealed in glass containers filled with (a) pure  $O_2$ , (b)  $N_2$ , and (c)  $H_2$ .

Table 1

Specific rates and kinetic constants of the slow reactions of gas evolution or consumption taking place in a VRLA system at open circuit

v <sub>s</sub> (kPa cm/h)	K <sub>Hs</sub> (cm/h)
$5 \times 10^{-2}$	
$7 \times 10^{-2}$ a	
	$5 \times 10^{-4}$
	6×10 <sup>-4</sup>
	(kPa cm/h) 5×10 <sup>-2</sup>

<sup>a</sup> Corresponding to about 0.04 mA/Ah.

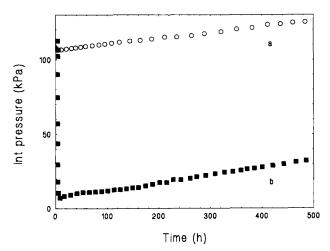


Fig. 6. Pressure vs. time plot for single negative plates, of the same kind, at open circuit in sealed glass containers filled with (a) pure  $N_2$  and (b) pure  $O_2$ .

appears constant within the first thousand of hours. In some exceptional cases,  $H_2$  evolution became par-

ticularly marked showing a rate one order of magnitude higher than that reported in Table 1: in such cases analysis of the active material revealed the presence of a higher amount of antimony.

Carrying out the tests on single negatives at open circuit in pure  $O_2$ , we found that at about a thousand of hours, pressure build-up slowed reaching a limit value of about 80 kPa. In those conditions all the initial  $O_2$  had been totally consumed, causing a slight discharge of the plate, and the internal volume of the glass case contained only  $H_2$  coming from the  $H_2$ -evolution reaction. The existence of an  $H_2$ -consuming process was therefore supposed.

Additional tests were carried out, in pure  $H_2$ , on single negatives both freshly charged and partially discharged. The results, reported in Fig. 7 curves (a) and (e), respectively, indicate that only  $H_2$  evolution is present in the case of the freshly charged plate while, in the case of the partially discharged one,  $H_2$  consumption takes place also, leading, when the  $H_2$  pressure reaches a sufficiently low value, to a steady-state situation. The curve for the empty glass case in  $H_2$ , curve (c), shows that the pressure variations reported in curve (e) do depend on the presence of the slightly discharged negative plate.

These findings suggest that  $H_2$  consumption is in some way related to the presence of PbSO<sub>4</sub> coming from the partial discharge of the plate. One can think to a possible reaction of  $H_2$  oxidation via the formation of sulfide-type compounds. At present it can only be noted that similar pressure tests in  $H_2$ , carried out on felt covered with sulfate and wetted with acid, showed the existence of an  $H_2$ -consuming process.

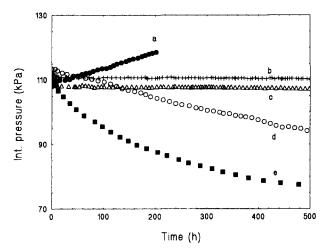


Fig. 7. Pressure vs. time plot for (a) a freshly charged negative in a sealed glass container initially filled with pure  $H_2$ , and (b) an empty battery case initially filled with pure  $N_2$ ; (c) an empty glass vessel initially filled with pure  $H_2$ ; (d) an empty battery case of the same type as (b) initially filled with pure  $H_2$ , and (e) a partially discharged negative of the same type and in the same conditions as (a).

Beyond these processes, we considered the passage of  $H_2$  across the plastic case of the batteries. The results show that the walls of the container act as a permselective membrane since  $H_2$  flows outwards even when the internal pressure is lower than the external, Fig. 7 curve (d). This phenomenon is typical of  $H_2$  only, as can be seen by comparing curves (b) and (d) in Fig. 7, its rate being related to the extension of the case walls surface.

# 4.2. Overcharge tests

Overcharge tests at constant current have also been accomplished on complete cells, fully charged and initially filled with pure  $N_2$ . The internal pressure increase during overcharge was limited by manually venting at 130 kPa until the pressure decreased to 100 kPa. The internal gas composition was periodically determined by gas chromatografic analysis of the vented gas.

An example of the results obtained is reported in Fig. 8 for an overcharge current of 2 A interrupted after 4 h for 2 h. At every opening of the vent plug the percentage of  $N_2$  lowers as it flows out. On the contrary, the moles of  $H_2$  and  $O_2$ , which are evolving, increase as the process goes on, tending to the molar ratio 2 to 1. During the open-circuit stage, the most important process is  $O_2$  consumption at the negatives. As a consequence, the  $O_2$  molar fraction lowers and that of  $H_2$  correspondingly increases.

In Fig. 8 are also reported the calculated values of the molar fractions obtained by applying the developed numerical method [17]. For all the batteries tested the fitting was at least as good as that reported in Fig. 8.

The time needed to reach the  $H_2/O_2$  ratio of 2, starting from pure  $N_2$ , depends on the rate of elimination of this gas, that is on the venting frequency which in

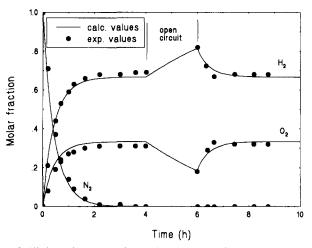


Fig. 8. Fitting of the experimental gas composition data for a cell (500 ml free volume, from a 12 V, 50 Ah battery) in overcharge at I=2A. Fitting parameters:  $K_0=0.4$  h<sup>-1</sup>;  $K_H=1\times10^{-4}$  h<sup>-1</sup>; spontaneous H<sub>2</sub>-evolution current=10 mA;  $f_H=f_0=f_N=0$  mol/h.

turn is proportional to the value of the overcharge current.

The behaviour of the cells under overcharge is strictly dependent on the state-of-charge of the plates. In conditions of fully charged positives and partially discharged negatives, most of the current at the negative plates goes into reduction of  $PbSO_4$ , so that the hydrogen/oxygen molar ratio is lower than 2 to 1.

Particularly interesting is the case in which a fully charged cell, initially filled with N<sub>2</sub>, is overcharged at a current intensity equal or lower than the O<sub>2</sub>-reduction limiting current [17,19]. At the beginning, Fig. 9(a),  $H_2$  and  $O_2$  evolution at the negative and positive plates occur. As the O<sub>2</sub> partial pressure builds up, the rate of O<sub>2</sub> recombination at the negative increases and, correspondingly, H<sub>2</sub> evolution decreases. The O<sub>2</sub> pressure attains in the end a value  $p_{\lim}$  at which the O<sub>2</sub>reduction limiting current becomes equal to the external current I,  $H_2$  evolution ceases and the pressure becomes constant. After a new venting, the total pressure will again increase to a constant value, lower than before. In fact the starting value of  $O_2$  partial pressure is, at every closing of the valve, higher, due to the progressive lowering of N<sub>2</sub> molar fraction, Fig. 9(c), so  $p_{lim}$  is reached at a lower value of the total pressure.

The transition from the  $O_2$ -consumption to the  $H_2$ evolution stage at the negatives is shown, at constant current, by the variation of cell potential. This shift is most marked when the limiting current for  $O_2$  reduction equals the external current, Fig. 10. Fig. 9(b) shows that at every venting, the cell potential rapidly moves to more positive values. This indicates the onset of  $H_2$ evolution at the negatives. When the valve is closed again the  $O_2$  moles number increases at a rate related

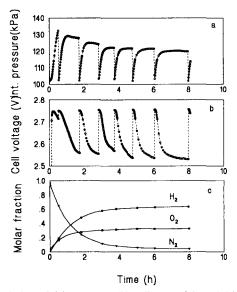


Fig. 9. Variation of (a) pressure, (b) cell potential, and (c) gaseous mixture composition for a cell (200 ml free volume, from a 12 V, 50 Ah battery) in overcharge at 0.5 A.

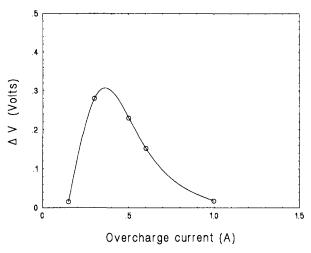


Fig. 10. Variation of the potential of a cell (200 ml free volume, from a 12 V, 50 Ah battery) at one of the valve openings during overcharge tests at various currents. The potential variation was measured when the gas composition inside the cell became constant, i.e. after about 8 h (see Fig. 9(a)).

to the external current I and the potential progressively lowers again.

# 4.3. Vent plugs

The experiments pointed out that the gas composition inside the cell is influenced not only by the current but also by the partial pressure of  $H_2$  and  $O_2$  as a consequence of periodic venting. We have therefore found it convenient from the technical viewpoint to investigate on the behaviour of the built-in vent valves of the cells considered.

The batteries were overcharged at constant current (from 1 to 5 A) for a time suitable to study the behaviour of the valves and then the circuit was opened while the internal pressure was being monitored. The plots in Fig. 11 refer to two of the cells under study in overcharge at 2 A. The opening pressure of the valve ranged in general between 110 and 130 kPa according to the type of cell and the overcharge current.

Curve (a) in Fig. 11 shows the behaviour of a correctly working vent plug. When, after the valve opening, the current is interrupted, the pressure decays very rapidly at the beginning, as long as the passage is still clear. After valve closing the internal pressure reaches values lower than atmospheric.

In the case of curve (b) in Fig. 11 it can be seen that, once opened, the valve does not close again completely, leaving the internal volume in communication with the outer ambient. This defect proved to be common to all the four types of accumulator, occurring in about 10% of the cells considered. The validity of these results is of course limited to the set of batteries used in the tests.

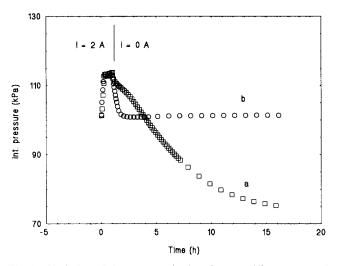


Fig. 11. Variation of the pressure in time for two different types of cell still equipped with the original vent plugs and in overcharge at 2 A.

#### 5. Conclusions

All the batteries considered in this work, showed a similar behaviour with respect to O<sub>2</sub> recombination, with a  $K_{Os}$  value for the cells tested around 0.04 cm/ h. Common is also the critical aspect regarding the limited reliability of the vent valves.

Comparison between the results of complete cells and couples of plates, giving a mean value of the merit factor of 0.06, has shown that the structural characteristics of the cells markedly limit the O2-recombination process.

Analysis of the pressure decay tests brought to conclude that  $O_2$  reduction is: (i) scarcely influenced by the presence of small quantities of sulfate, and (ii) affected by local temperature variations and/or water flux.

Evidence was found for four slow rate processes, whose rate is of the order of  $10^{-2}$  kPa/h. One of them is a reaction of  $H_2$  consumption at a slightly discharged negative plate, which is apparently related to the lead sulfate presence at the plate surface.

Finally, it has been found that  $H_2$  flows through the case walls at a rate comparable with that of the slow reactions considered and that the walls act as permselective membranes.

The overcharge tests with internal pressure, gas composition and cell potential monitoring provided a further verification of the suitability of the proposed mathematical model. The results indicate that the pressure variations due to venting exert their influence both on gas composition and on cell potential, particularly when the conditions are so that O<sub>2</sub>-limiting current equals the external one ( $\Delta V_{\text{max}} = 300 \text{ mV}$ ).

From the analysis of the whole set of overcharge tests we came to the conclusion that the  $H_2/O_2$  molar ratio in a battery submitted to a current can be lower than 2 when the negatives are not completely charged. It can be higher than 2 when: (i) low  $H_2$  overpotential impurities are present; (ii) the corrosion process at the positive grids is not negligible, and (iii) the negatives do not behave uniformly.

### 6. List of symbols

- F Faraday's constant
- gas leaks through the battery container (mol/  $f_{\rm H}, f_{\rm N}, f_{\rm O}$ h)
- I external current (A)
- $I_{c}$ corrosion current at the positive plate (A)
- $I_{\rm H}, I_{\rm O}$  $H_2$ -evolution current at the negative and  $O_2$ evolution current at the positive, due to the external current (A)
- $K_{\rm H}, K_{\rm O}$ kinetic constants for the reactions of  $H_2$  and  $O_2$  consumption at the positive and negative plates  $(h^{-1})$
- KHS, KOS kinetic constants referred to the unit of free volume and geometric plate surface (cm/h)
- $N_{\rm H}, N_{\rm O}$ number of  $H_2$  and  $O_2$  moles in the cell free volume at time  $t \pmod{t}$
- cell internal pressure (kPa) р
- value of the  $O_2$  partial pressure at which,  $p_{lim}$ during the overcharge tests, the O<sub>2</sub>-limiting current becomes equal to the external current I (kPa)
- $S_n, S_p$ total geometric area of the negative and the positive plates in a complete cell or in a couple of plates (cm<sup>2</sup>)
- time (h) t
- Ttemperature (K)
- $v_{s} V$ specific reaction rate (kPa cm/h)
- free volume of the cell (cm<sup>3</sup>)
- $\Gamma_{\rm o}$ merit factor for O<sub>2</sub> reduction at the negative

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